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% The 4th Nonlinear CAE Seminar
% Exercise 2 using Newton's Method
%
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%
%-----
% Material Properties
E=5*10^9; v=0.3;
%
% Geometry of the string
L=0.5;
d=0.002;
A=pi*d^2/4;
%
% Applied forces
b=10*9.81;
P=3.1*9.81;
%
% Order of polynomials and d.o.f.
p=2;
dof=p+1;
%
%-----
% Pre-processing: Create an FEM model
%-----
% # of elements, # of nodes, # of total d.o.f.
nelx=10;
nx=nelx*p+1;
dx=L/(nx-1);
neq=nx*2;
%
% Element connectivity
ijk=zeros(nelx,dof);
for i=1:nelx
    for j=1:dof
        ijk(i,j)=(i-1)*p+j;
    end
end
%
% Nodal coordinates
xG=zeros(nx,2);
for i=1:nx
    xG(i,1)=(i-1)*dx;
end
%
% Plot model
%
xo=zeros(1,2); yo=zeros(1,2); icont=[1,p+1];
for nel=1:nelx
    if nel==2, hold, end
    %
    for jj=1:2
        j=ijk(nel,icont(jj));
        xo(jj)=xG(j,1);
        yo(jj)=xG(j,2);
    end
    plot(xo,yo)
    %
end
hold off
pause

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%
%-----
% Define boundary and loading conditions
%-----
% Boundary conditions (Simply supported)
ndc=2;
dcnode=[1,1,1,0,0;
        nx,0,1,0,0];
%
% Loading conditions
fg1=zeros(nx,1);
fg2=zeros(nx,1);
%
% Tensile point load at the roller
fg1(nx,1)=P;
%
% Distributed load in the transverse direction
if p==1
    imax=2; a=1/sqrt(3);
    gwi=[1,1]; gxi=[-a,a];
elseif p==2
    imax=3; a=sqrt(3/5);
    gwi=[5,8,5]/9;gxi=[-a,0,a];
end
%
for nel=1:nelx
    %
    xge=zeros(1,2);
    ideg=zeros(1,dof);
    %
    xge(1)=xG(ijk(nel,1),1);
    xge(2)=xG(ijk(nel,1+p),1);
    %
    for i=1:dof
        ideg(i)=ijk(nel,i);
    end
    %
    fge=zeros(dof,1);
    for ig=1:imax
        gw1=gwi(ig); r=gxi(ig);
        %
        Le=xge(2)-xge(1);
        J=Le/2;
        %
        if p==1
            NF=[1-r,1+r]/2;
        elseif p==2
            NF=[r*(r-1)/2,1-r^2,r*(r+1)/2];
        end
        fge=fge+NF'*b*J*gw1;
    end
    for i=1:dof
        fg2(ideg(i))=fg2(ideg(i))+fge(i);
    end
end
%
%-----
% Construct tangent stiffness matrix
%-----
%
Ug=zeros(2*nx,1);

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%
lt=0;
%for lt=1:5
%
enorm=1;
while enorm > 10^-3;
lt=lt+1
%
K11=zeros(nx);
K12=zeros(nx);
K22=zeros(nx);
Qg1=zeros(nx,1);
Qg2=zeros(nx,1);
%
% Element tangent stiffness matrix
for nel=1:nelx
%
xge=zeros(1,2);
ideg=zeros(1,dof);
%
xge(1)=xG(ijk(nel,1),1);
xge(2)=xG(ijk(nel,1+p),1);
%
for i=1:dof
ideg(i)=ijk(nel,i);
end
%
ue=zeros(dof,1);
ve=zeros(dof,1);
for i=1:dof
ue(i)=Ug(ideg(i));
ve(i)=Ug(nx+ideg(i));
end
%
ske11=zeros(dof);
ske12=zeros(dof);
ske22=zeros(dof);
qe1=zeros(dof,1);
qe2=zeros(dof,1);
%
for ig=1:imax
gw1=gwi(ig); r=gxi(ig);
%
Le=xge(2)-xge(1);
J=Le/2;
%
if p==1
NF=[1-r,1+r]/2;
B=[-1,+1]/2/J;
elseif p==2
NF=[r*(r-1)/2,1-r^2,r*(r+1)/2];
B=[r-1/2,-2*r,r+1/2]/J;
end
%
Nxp=E*A*((B*ue)+(B*ve)^2/2);
%
ske11=ske11+B'*Nxp+E*A*(1+B*ue)^2*B*J*gw1;
ske12=ske12+B'*E*A*(1+B*ue)*(B*ve)*B*J*gw1;
ske22=ske22+B'*Nxp+E*A*(B*ve)^2*B*J*gw1;
%
qe1=qe1+B'*Nxp*(1+B*ue)*J*gw1;

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    qe2=qe2+B'*Nxp*(B*ve)*J*gw1;
end
%
% Assembly
for i=1:dof
    Qg1(ideg(i))=Qg1(ideg(i))+qe1(i);
    Qg2(ideg(i))=Qg2(ideg(i))+qe2(i);
    for j=1:dof
        K11(ideg(i),ideg(j))=K11(ideg(i),ideg(j))+ske11(i,j);
        K12(ideg(i),ideg(j))=K12(ideg(i),ideg(j))+ske12(i,j);
        K22(ideg(i),ideg(j))=K22(ideg(i),ideg(j))+ske22(i,j);
    end
end
end
%
if It==1
    % Initial guess (linear tensile solution)
    %
    % Apply boundary condition
    kdeg=linspace(1,nx,nx);
    bdeg=[];
    k=0;
    for i=1:ndc
        if dcnode(i,2) ~= 0
            k=k+1;
            bdeg(k)=dcnode(i,1);
            kdeg(bdeg(k))=0;
        end
    end
    end
    %
    kdeg(bdeg)=[];
    K11(bdeg,:)=[];
    K11(:,bdeg)=[];
    fg=fg1;
    fg(bdeg)=[];
    %
    % Solve linear equations
    ug=inv(K11)*fg;
    for i=1:nx-k
        Ug(kdeg(i))=ug(i);
    end
    % Error norm (energy)
    enorm=fg'*ug
    %
    %
else
    %
    skg=[K11,K12;K12',K22];
    fg=[fg1-Qg1;fg2-Qg2];
    %
    % Apply boundary conditions
    kdeg=linspace(1,neq,neq);
    bdeg=[];
    k=0;
    for i=1:ndc
        for j=1:2
            if dcnode(i,j+1) ~= 0
                k=k+1;
                bdeg(k)=mod(j+1,2)*nx+dcnode(i,1);
                kdeg(bdeg(k))=0;
            end
        end
    end
end

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    end
end
%
kdeg(bdeg)=[];
skg(bdeg,:)=[];
skg(:,bdeg)=[];
fg(bdeg)=[];
%
% Solve linearized equations for increments
ug=inv(skg)*fg;
for i=1:neq-k
    Ug(kdeg(i))=Ug(kdeg(i))+ug(i);
end
% Error norm
%norm(ug)
enorm=fg'*ug
%
%-----
% Plot model
%
xo=zeros(1,dof); yo=zeros(1,dof);
xp=zeros(1,dof); yp=zeros(1,dof); icont=linspace(1,dof,dof);
%
for nel=1:nelx
    if nel==2, hold, end
    %
    for jj=1:dof
        j=ijk(nel,icont(jj));
        xo(jj)=xG(j,1);
        yo(jj)=xG(j,2);
        xp(jj)=xG(j,1)+Ug(j);
        yp(jj)=xG(j,2)+Ug(nx+j);
    end
    plot(xo,yo,':',xp,yp,'o',xp,yp)
    %
end
axis equal
%axis off
hold off
pause
%
if It > 20, enorm=0; 'Non-convergent after 20 iterations!', end
%
end
%
end
%
%-----
% Green-Lagrange Strain in each element
Ex=zeros(nelx,2);
for nel=1:nelx
    xge=zeros(2,1);
    ideg=zeros(1,dof);
    %
    xge(1)=xG(ijk(nel,1),1);
    xge(2)=xG(ijk(nel,1+p),1);
    %
    for i=1:dof
        ideg(i)=ijk(nel,i);
    end
end
%
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ue=zeros(dof,1);
ve=zeros(dof,1);
for i=1:dof
    ue(i)=Ug(ideg(i));
    ve(i)=Ug(nx+ideg(i));
end
%
r=0; %Strain evaluated at element center
%
Le=xge(2)-xge(1);
J=Le/2;
%
if p==1
    NF=[1-r,1+r]/2;
    B=[-1,+1]/2/J;
elseif p==2
    NF=[r*(r-1)/2,1-r^2,r*(r+1)/2];
    B=[r-1/2,-2*r,r+1/2]/J;
end
% Green-Lagrange Strain Ex
Ex(nel,1)=B*ue+((B*ue)^2+(B*ve)^2)/2;
%
% Strain calculated from change in element length: Ex=(ds^2-dS^2)/dS^2/2
ds=norm([Le+ue(dof)-ue(1),ve(dof)-ve(1)]);
dS=Le;
Ex(nel,2)=(ds^2-dS^2)/dS^2/2;
end

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